INTERACTION OF A SYSTEM OF GRIFFITH CRACKS IN AN ELASTO-BRITTLE MATERIAL

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Zhurnal Prikladnoi Mekhaniki i Tekhnicheskoi Fiziki, Vol. 7, No. 5, pp. 163-166, 1966

Problems of the theory of cracks have recently attracted a great deal of attention. Finding accurate solutions for systems of cracks presents considerable mathematical difficulties. An approximate solution of a static problem of the theory of equilibrium cracks is given in [1]. The hypothesis formulated in [1] is used in this article in which the problem of interaction of Griffith cracks in an elasto-brittle material is analyzed and the accuracy of the solution obtained is estimated.

Let an infinite isotropic body contain an infinitely large number of cracks of a length 2l, parallel to the axis of abscissas and spaced at a distance of 2h from each other. A constant pressure p is acting inside each crack along the length 2l. In view of the symmetry of the system, our considerations may be confined to a band  $0 \le y \le h$  whose lower edge coincides with the longitudinal crack axis, its upper edge being halfway between two adjacent cracks. The problem is to find the relationship between p, h and l if all the elastic constants and the cohesion modulus are known.

Let us consider plane deformation. In this case the stress tensor components  $\sigma_X$ ,  $\sigma_y$ , and  $\sigma_{Xy}$  and displacement vector components u and v are expressed through two analytical functions  $\varphi(z)$  and  $\psi(z)$  and their derivatives by the Kolosov-Kuskhelishvili formulas:

$$\sigma_x + \sigma_y = 2 \left[ \varphi'(z) + \overline{\varphi'(z)} \right], \tag{1}$$

$$\sigma_y - \sigma_x + 2i\sigma_{xy} = 2 \left[ \vec{z} \varphi^{\prime \prime} \left( z \right) + \psi^{\prime} \left( z \right) \right], \tag{2}$$

$$2\mu (a + iv) = \varkappa \varphi (z) - z \overline{\varphi'(z)} - \overline{\psi(z)} \qquad (\varkappa = 3 - 4v). \quad (3)$$

Here v is the Poisson ratio and  $\mu$  shear modulus. The boundary conditions will be

$$\sigma_y = -p \quad (y = 0, \quad -l \leqslant x \leqslant +l), \tag{4}$$

$$\sigma_{xy} = 0$$
  $(y = 0, y = h, -\infty < x < +\infty),$  (5)

$$v = 0 \quad \begin{cases} (y = 0, -\infty < x < -l, +l < x < +\infty) \\ (y = h, -\infty < x < +\infty). \end{cases}$$
(6)

The stress tensor components at infinity behave as

$$\sigma_{ij}(r) = o(r^{-1}) \quad \text{at} \quad r \to \infty.$$
(7)

Introducing in accordance with [1] an assumption

$$\sigma_x = \sigma_y \quad \text{at} \quad y = 0 , \tag{8}$$

we can formulate the problem in terms of one analytical function  $\varphi'(z)$ :

Re 
$$\varphi'(z) = -\frac{1}{2}p$$
  $(y = 0, -l \le x \le +l)$   
Im  $\varphi'(z) = 0$   $(y = 0 - \infty < x < -l,$   
 $+ l < x < +\infty)$   
Im  $\varphi'(z) = 0$   $(y = h, -\infty < x < +\infty)$ . (9)

A conformal mapping of the band  $0 \le y \le h$  on the upper semiplane (Fig. 2) is given by

$$\tau = e^{\pi z/h} \,. \tag{10}$$

In the semi-plane  $\eta > 0$  we obtain the complex Keldysh-Sedov boundary problem [3].

The unknown analytical function  $\varphi'(z)$  should have singularities of the order of  $x^{-1/2}$  at points z = l and z = +l approached from the left and right, respectively, and the coefficients at these singularities should – in view of the symmetry of the problem – be equal. A solution satisfying these conditions is in the form

$$\begin{split} \varphi'(z) &= -\frac{p}{2} \left\{ 1 - \frac{\sqrt[4]{a}}{a+1} \left[ \sqrt[4]{a} \left( \frac{e^{\pi z/h} - a^{-1}}{e^{\pi z/h} - a} \right)^{1/z} + \frac{1}{\sqrt{a}} \left( \frac{e^{\pi z/h} - a}{e^{\pi z/h} - a^{-1}} \right)^{1/z} \right] \right\} \,. \end{split}$$
(11)

Using Eqs. (8) and (1), we find that at the crack tips  $\sigma_y$  has singularities in the form

$$(-l-x) = \sigma_y (l+x) = \frac{N}{\sqrt{x}} - \frac{p}{2} + O(x^{3/2}),$$
$$N = p \left(\frac{h}{\pi}\right)^{1/2} \left(\frac{e^{\pi l/h} - 1}{e^{\pi l/h} + 1}\right)^{1/2}.$$
(12)

In accordance with [4] we have an equation

$$p\left(\frac{h}{\pi}\right)^{1/2} \left(\frac{e^{\pi l/h} - 4}{e^{\pi l/h} + 1}\right)^{1/2} = \frac{K}{\pi} , \qquad (13)$$

where K is the cohesion modulus.

 $\sigma_{u}$ 

Equation (13) determines the values of p corresponding to the limiting equilibrium of the system of cracks under consideration. After some elementary transformations we obtain an expression relating the half-length of an equilibrium crack to p and h

$$l = \frac{h}{\pi} \ln \frac{p^2 + K^2 / \pi h}{p^2 - K^2 / \pi h} .$$
 (14)

At the limit, i.e., at  $h \rightarrow \infty$ , we obtain an expression cited in [4],

$$l = 2K^2 / \pi^2 p^2 \tag{15}$$

relating to an isolated Griffith crack.

It follows from Eq. (14) that for any finite h the pressure p corresponding to infinitely large crack lengths l approaches its critical value

$$p_* = \frac{1}{\sqrt{\pi h}} K ,$$

which increases with decreasing h, while from Eq. (15) it follows that at large l the pressure  $p \rightarrow 0$ .

It follows from Fig. 3 that a system of Griffith cracks spaced at 2h intervals can exist only when  $p > p_*$ . At  $p < p_*$  reversible cracks close up. At equal values of p acting inside cracks, the length of an isolated crack will be smaller than that of a crack in a system of cracks. The pressure p which at a finite h corresponds to the limiting equilibrium is larger for a system of cracks than for an isolated crack (of the same length), this being the way in which the interaction of a system of cracks is manifested.

From Eqs. (1) and (2) we obtain

$$\sigma_y = 2\operatorname{Re}\phi'(z) + \operatorname{Re}\left[\bar{z}\phi''(z) + \psi'(z)\right],$$
  
$$\sigma_x = 2\operatorname{Re}\phi'(z) - \operatorname{Re}\left[\bar{z}\phi''(z) + \psi'(z)\right]. \quad (16)$$

Taking into account that  $\sigma_{xy} = 0$  at y = 0, we find that the hypothesis [8] is equivalent to an equation

$$\bar{z}\phi''(z) + \psi'(z) = 0$$
 at  $y = 0$ 

which is rigorously satisfied only in the case of a single crack.



Fig. 1





Fig. 3











In the case of a system of cracks Re  $[\bar{z}\phi''(z) + \psi'(z)]$  characterizes the redistribution of stress due to the presence of adjacent cracks. Let us find the values of the ratio l/h at which the above obtained approximate solution may be used.

To this end let us formulate a problem for which an accurate solution can be found.

Consider an infinitely elastic body containing a system of parallel Griffith cracks. Stresses acting in the body are such that along each crack  $\sigma_x + \sigma_y = -2p$ . The cracklength and the spacing between cracks are 21 and 2h, respectively. In view of the symmetry of the problem let us consider only the band  $0 \le y \le h$ .

The boundary conditions will be

$$\sigma_{x} + \sigma_{y} \approx -2p \quad (y = 0, -l \leqslant x \leqslant + l) \sigma_{xy} = 0 \quad (y = 0, y = h, -\infty < x < +\infty) v = 0 \begin{cases} (y = 0, -\infty < x < -l, +l < x < +\infty) \\ (y = h, -\infty < x < +\infty). \end{cases}$$
(17)

When the problem is formulated in this way, its accurate solution is in the form of Eq. (11) which determines the function  $\varphi'(z)$ .

At y = 0 the values of the function  $\bar{z}\varphi''(z) + \psi'(z)$  coincide with the values of an analytical function  $z\varphi''(z) + \psi'(z)$  in the region in question, since  $z = \bar{z}$  at y = 0. From Eq. (2) it is easy to obtain

$$\sigma_{xy} = \operatorname{Im} \left[ \bar{z} \varphi^{\prime \prime} \left( z \right) + \psi^{\prime} \left( z \right) \right]. \tag{18}$$

From the boundary condition  $\sigma_{xy} = 0$  at y = h we have

Im 
$$[z\varphi''(z) + \psi'(z)] = 2h \operatorname{Re} \varphi''(z)$$
 (19)

At y = 0 from the condition  $\sigma_{XY} = 0$  we have

Im 
$$[z\phi''(z) + \phi'(z)] = 0.$$
 (20)

Let us denote by  $F(\zeta)$  an analytical function corresponding to the function  $z\varphi''(z) + \psi'(z)$ . After mapping the band  $0 \le y \le h$  on the upper semi-plane  $\eta > 0$ , we obtain the Dirichlet problem with the following boundary conditions:

$$\operatorname{Im} F(\xi) = u(\xi) \qquad (-\infty < \xi \le 0) \\
\operatorname{Im} F(\xi) = 0 \qquad (0 \le \xi < +\infty) .$$
(21)

Using (11) and following [2], we obtain a function  $u(\boldsymbol{\xi})$  in the form

$$u(\xi) = \frac{p}{4}\pi[2-A] \frac{\xi(\xi+1)}{\left[\xi^2 - \xi A + 1\right]^{3/2}} \quad \begin{pmatrix} A = a + a^{-1} \\ A \ge 2 \end{pmatrix}.$$
(22)

The solution of the problem studied will be

$$F(\zeta) = -\frac{p}{4} [2 - A] \left\{ \frac{2\zeta}{\zeta^2 - \zeta A + 1} + \zeta (\zeta + 1) \chi (\zeta) \right\}.$$
 (23)

It should be pointed out that the function  $\chi(\zeta)$  has two branches since it is described by an integral of the following type:

$$\int \frac{dx}{\sqrt{ax^2 + bx + c}}$$

The above integral has several branches depending on the sign of aand  $\Delta \approx ac - b^2$ . At  $-\infty < \xi < (a^{-1})$ ,  $a < \xi < +\infty$ , when  $\xi^2 - \xi = \xi$   $(a + a^{-1}) + 1 > 0$ , we have

$$\chi(\xi) = \frac{1}{(\xi^2 - \xi A + 1)^{3/2}} \times \left[ 2 \ln \frac{\sqrt{a\xi - 1} + \sqrt{\xi/a - 1}}{\sqrt{\xi - a} + \sqrt{\xi - a^{-1}}} - \ln \xi \right].$$
(24)

At  $1/a < \xi < a$ , when  $\xi^2 - \xi (a + 1/a) + 1 < 0$ , we have

$$\chi(\xi) = \frac{-1}{(\xi^2 - \xi A + 1)(-\xi^2 + \xi A - 1)^{1/2}} \times \\ \times \left[ \arcsin \frac{A - 2\xi^{-1}}{VA^2 - 4} - \arcsin \frac{2\xi - A}{VA^2 - 4} \right].$$
(25)

The solution obtained should have no singularities at the crack tips. Assuming  $\xi = a - s$  and  $\xi = a + s$  and doing some simple transformations, it is easy to prove that this is so.

Figure 5 shows that along a segment of the real axis  $1/a \le \le \le a$  the function F(5) has a maximum at the point  $\xi = 1$  (which in the plane x, y corresponds to the point z = 0).

When l is finite and  $h \rightarrow \infty$ , the following is true:

$$a \approx 1 + s + \frac{s^2}{2!} + \frac{s^3}{3!} + \frac{s^4}{4!}$$

$$\frac{1}{a} \approx 1 - s + \frac{s^2}{2!} - \frac{s^3}{3!} + \frac{s^4}{4!}$$
(26)

Passing in Eqs. (23) and (24) to the limit at  $h \rightarrow \infty$  and taking into account Eq. (26), we obtain

$$F(1) \sim (l/h)^2.$$
 (27)

Consequently,  $F(\zeta) \rightarrow 0$  at  $h \rightarrow \infty$ , the solution obtained approaches the solution for a single Griffith crack.

In can be concluded from Fig. 6 that the approximate solution, accurate to 10%, will be valid for ratios  $l/h \leq 0.5$ .

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